

# Problem with using a single multiplier for LOFT

Neil Birkett

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## Background

LOFT calibration currently utilizes a filtered detector to determine the presence of LOFT and IQ imbalance. The detector output is subsequently digitally downconverted and filtered to obtain a 5MHz or 10MHz tone. In the original design, the frequency translation is done using a single mixer. This is shown in Figure 1.

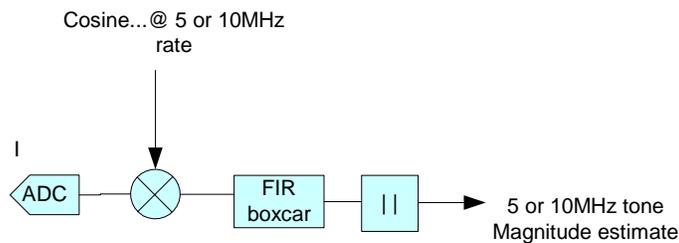


Figure 1 Digital down conversion and filtering to obtain an estimate of the magnitude of the detector 5 or 10MHz tone.

## Math

Let the detector signal be represented by

$$S_d = A \cos(\omega_c t + \varphi_d) \quad \text{Equation 1}$$

Where  $A$ ,  $\omega_d$  and  $\varphi_d$  are the magnitude and frequency of the detected filtered signal respectively and  $\varphi_d$  is the phase of the detected signal with respect to the mixer local oscillator.

The phase  $\varphi_d$  is comprised of two parts,

- a fixed phase  $\varphi_{gd}$  due to absolute group delay between the transmitted tones and the sampled baseband.
- A relative phase delay  $\varphi_r$  due to the magnitude of individual I and Q DC offsets.

$$\varphi_d = \varphi_{gd} + \varphi_r \quad \text{Equation 2}$$

The relative phase delay  $\varphi_r$  is described by the following equation;

$$\varphi_r = \tan^{-1}\left(\frac{Q_{DC}}{I_{DC}}\right) \quad \text{Equation 3}$$

Let the digital multiplying tone be represented by

$$S_m = \cos(\omega_d t) \quad \text{Equation 4}$$

The resultant signal after multiplication is;

$$S_r = A \cos(\omega_c t + \varphi_d) \cos(\omega_d t) = \frac{A}{2} [\cos(\varphi_d) + \cos(2\omega_d t + \varphi_d)] \quad \text{Equation 5}$$

After filtering, the double frequency components are removed so that the signal can be represented by;

$$S_{out} = \frac{A}{2} \cos(\varphi_d) = \frac{A}{2} \cos(\varphi_{gd} + \tan^{-1}\left(\frac{Q_{DC}}{I_{DC}}\right)) \quad \text{Equation 6}$$

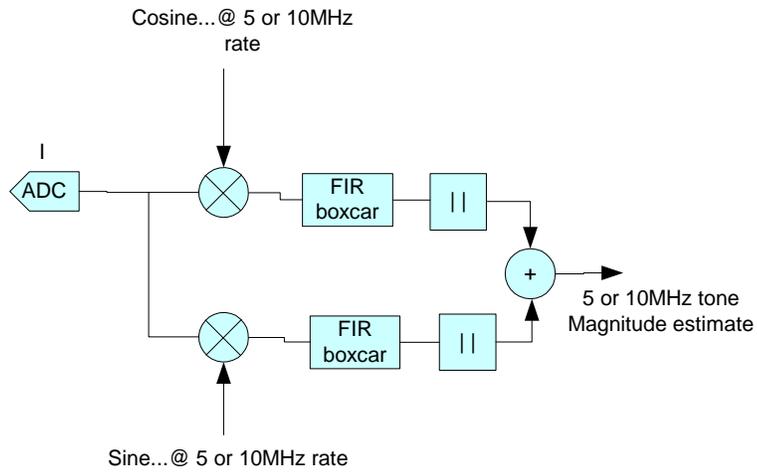
### ***Problem with the single downconversion***

***Equation 4 illustrates the problem.*** Basically, the phase of the detected signal relative to the multiplying signal can result in a zero (or small magnitude) output from the filter if  $\varphi_d$  is close to 90 degrees. It is compounded by the fact that the phase of 5MHz signal out of the detector is also dependent on the individual magnitudes of the I-path DC and Q-path DC offsets. As well, the  $S_{out}$  value will have a polarity associated with it depending on the phase  $\varphi_d$ .

An I path DC offset will create a 5MHz detector tone which is 90 degrees out of phase with that generated by a Q path DC offset. This means that in real situations, the magnitude of the downconverted DC signal (i.e. the error signal) will wander according to how much I and Q path DC offset there is, and this changes the phase of the detector signals with respect. Unfortunately we have no control over this.

### ***Solution to the problem***

One solution to the problem is to implement a *quadrature* downconversion in digital, which would require multiplications using digital cosine and sine multiplying functions and a magnitude function. Instead of a magnitude function, a reasonable estimate can be obtained by using absolute values. Figure 2 illustrates this technique.



**Figure 2. Quadrature conversion eliminates magnitude wandering due to phase variation.**